

PERFORMANCE OPTIMISATION AND COST REDUCTION THROUGH ADVANCED PROCESS CONTROL



Basic Process Control

- Flow pacing
- Feedback control using PID loops
 - pH
 - Free available chlorine

Advanced Process Control (APC)

$$\begin{aligned}
 & |D(T, \epsilon, a, b)| \leq 2 \\
 & \varphi(5_1 t) \varphi(5_2 t) = \varphi(\sqrt{5_1^2 + 5_2^2} t) \\
 & \sum_{k=1}^r \int_{b_k \epsilon}^{x+b_k \epsilon} \left(\int_0^t \Psi_k^*(\tau) d\tau \right) dt - x \int_0^{b_k \epsilon} \Psi_k^*(\tau) d\tau = \frac{x^2}{2} B(v) + \int_0^x (x-u) \sum_{k=1}^r p_k^*(u) du \quad A(v) = \sum_{k=1}^r b_k \Psi_k^*(b_k \epsilon v) \\
 & P(x) = \frac{\sum_{k=1}^r p_k^* \log_2 \frac{1}{p_k}}{\sum_{k=1}^r p_k^*} \quad C_{lk} \overline{5_k} = 2 \cdot C_{lk} \\
 & y = \phi(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{+\infty} e^{-\frac{t^2}{2}} dt \quad h_1 = \sum_{k=1}^r a_k \overline{5_k} \quad \log \varphi(u) = -\frac{5^2 u^2}{2} \quad i^2 = -1; j^2 = -1; k^2 = -1 \\
 & S(\alpha, t) = \frac{2}{\pi} \int_0^t \frac{\sin \alpha t}{t} dt \quad P(\eta_\infty < x) = F(x) \quad \lim_{n \rightarrow \infty} \frac{\binom{2n}{n}}{(2n)!} = e^{-2x} \\
 & W_h = \left(\frac{h}{h} \right) p^h (1-p)^{h-h} \quad P(\eta < y | \xi = x) = \sup_{y' < y, y' \neq x} P(\eta < y' | \xi = x) \\
 & S_n = A_n U T A_n \quad f(t|y) = \frac{2e^{\frac{y^2}{2}}}{\sqrt{2\pi}} \int_{-\infty}^t \frac{e^{-\frac{u^2}{2}} du}{(1-\frac{y^2}{u^2})^{\frac{3}{2}}} \quad \sum_{n=1}^N \frac{\epsilon_n}{n} \\
 & |A_n| = \frac{n!}{2} \left| \int_{|x|>A} f(x) \log_2 \frac{1}{f(x)} dx \right| < \epsilon \quad g^{-1} \cdot g = e \quad y = \sqrt{\frac{\lambda_n}{\nu_n}} \left(\frac{\eta_{2n}}{\nu_n} + \frac{\eta_{2n} - \eta_{2n}}{\nu_n} \right) \quad H_r(x) = \frac{G_r(x)}{1+G_r(x)} \quad \sum_{n=1}^N \frac{1}{n} \\
 & \prod_{i=1}^{n-1} M_i; \bigcup_{i=1}^n X_n \quad f_n(t) = \frac{2^n t^{n-1} e^{-2t}}{(n-1)!} \quad U_n^{+} = \binom{2n}{n} - \binom{2n}{n-c} \\
 & \int_{-\infty}^{+\infty} dG_n(x) \geq \frac{1}{2} \sum_{a=-\infty}^{+\infty} e^{-\frac{|a-\mu|^2}{2}} = H(a) \quad \lim_{n \rightarrow \infty} \frac{\eta_n}{n} = P_e \quad R = \int_{-\infty}^{+\infty} \varphi(t) dt \\
 & f_{n-1}(t) = \int_0^t f_n(u) f_1(t-u) du = \frac{2^{n+1} t^n e^{-2t}}{n!} \quad \lim_{t \rightarrow 0} (Rt) = 0 \quad \lim_{n \rightarrow \infty} \frac{\eta_n}{n} = P_e \quad \int_{-\infty}^{+\infty} \sinh \left[\varphi(t) e^{-itx} + \varphi(-tx) \right] dt \\
 & \log \varphi(t) = i g(t) - c |t|^\alpha \left[1 + i \beta \frac{t}{|t|} \omega \log |t| \right] \quad B(v) = \sum_{k=1}^r \Psi_k^*(b_k v) \quad C_{iv} = \sum_{j=1}^r a_{ij} b_j v \quad C_n(\alpha) \geq \frac{n!}{\prod_{k=1}^n n_k(\alpha)!} \quad \frac{1}{m} \varphi(t) = \varphi(c(\frac{n}{m})t) \\
 & \int_{-\infty}^{+\infty} e^{-\frac{u^2}{2}} du = F(x) \left(\frac{1}{\sqrt{2\pi}} \right)^{-1} \quad |\psi_s(t)| = \left| \int_{-\infty}^{\infty} e^{itx} dF(x) \right| \leq \int_{-\infty}^{\infty} e^{-vx} dF(x) = \varphi_s(v) \quad g^{-1} N_g = \{g^{-1} n g \mid n \in N\} \quad Q = F^{-1}(q) \quad q_n(\alpha) = \frac{p_n^\alpha}{\sum_{j=1}^r p_j^\alpha} \quad PC(\Pi_2) = \sum_{j=1}^r p_j^\alpha \\
 & \prod_m = \prod_l \prod_{m-l} \quad \lim_{n \rightarrow \infty} \frac{1}{n} \ln \left(\frac{x}{\ln n} \right) = \frac{1}{\sqrt{2\pi}} e^{-\frac{x^2}{2}} \quad P_n(b) = \frac{c_n}{p_n} \quad P(\lim_{n \rightarrow \infty} \sup \frac{|\ln n|}{\sqrt{2n \log \log n}} \leq 1) = 1 \quad (\varphi(t) = 1 - \sqrt{1 - e^{-2it}}) \\
 & f: X \rightarrow X \cap W \quad f g(u_i) = f \left(\sum_{j=1}^{\dim V_2} a_{ji} v_j \right) = \sum_{j=1}^{\dim V_2} a_{ji} \left(\sum_{k=1}^{\dim V_2} b_{kj} w_k \right) \frac{\binom{2k}{2}}{2^{2k}} \approx \frac{1}{\sqrt{\pi} l^2} \\
 & Q(A) = \int_A \chi(\omega) dP \quad l'(\alpha) = -\log_2 \left(\frac{\sum_{k=1}^r p_k^* \log_2 \frac{1}{p_k}}{\sum_{k=1}^r p_k^*} - \left(\frac{\sum_{k=1}^r p_k^* \log_2 \frac{1}{p_k}}{\sum_{k=1}^r p_k^*} \right)^2 \right) \quad P_{j,r}^{(m)} = \sum_{e=0}^{\infty} P_{je}^{(r)} P_{ek}^{(m-r)} \quad \frac{1}{2\pi} \int_{-\infty}^{\infty} \operatorname{Re} \left\{ \varphi(t) \frac{e^{ita} - e^{itb}}{it} \right\} dt \\
 & q \left(e^{-x} \sqrt{\frac{1-q}{nq}} - 1 \right) = x \sqrt{\frac{q(1-q)}{n}} + O(\frac{1}{n}) \quad \prod_{k=1}^r \left[g_k \left(\frac{t}{\sqrt{N_k}} \right) \right]^{\lambda_k} = e^{-\frac{t^2}{2}} \quad P(|\Delta N| > \epsilon) \leq \frac{C_q}{\log N} \\
 & \liminf_{N \rightarrow \infty} \int_{-\infty}^{+\infty} f_N(x) dx \geq \int_{-\infty}^{+\infty} f(x) dx \quad M(1/\delta_f - 1/\delta_s) = \int_0^{\infty} (x-1)^{\delta_f} e^{-x} dx \quad \lim_{N \rightarrow \infty} \int_{-1}^1 f_N(x) \log_2 \frac{1}{f_N(x)} dx = \int_{-1}^1 f(x) \log_2 \frac{1}{f(x)} dx \\
 & D^2(J_n) \leq \frac{K}{n} + 2K \left(\frac{1}{L} \sum_{k=1}^r R(k) \right) \quad \det(M') = \det(M) + \det(M^*) = \det(M) \quad h(x,y) = \frac{1}{2\pi} \left[\left(\frac{1}{2} e^{-\frac{x^2}{2}} - e^{-xy} \right) \right] \quad |M(\epsilon_n, \epsilon_m)| \leq C_2 \sqrt{\frac{n}{m-n}}
 \end{aligned}$$

APC Examples

- Feed forward control
- Indirect sensors
- Sequential logic control
- Model predictive control





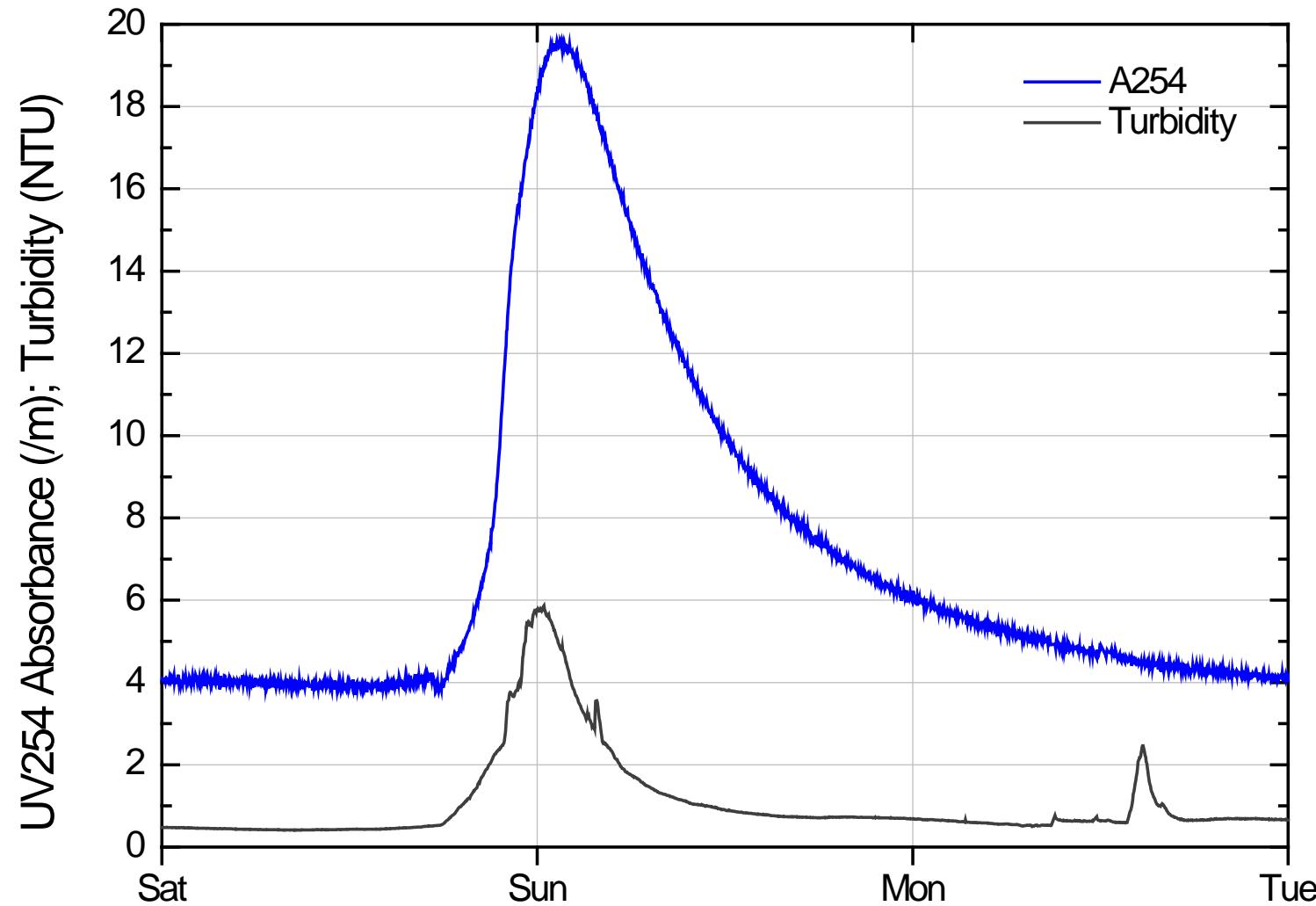
Challenges at the Plant

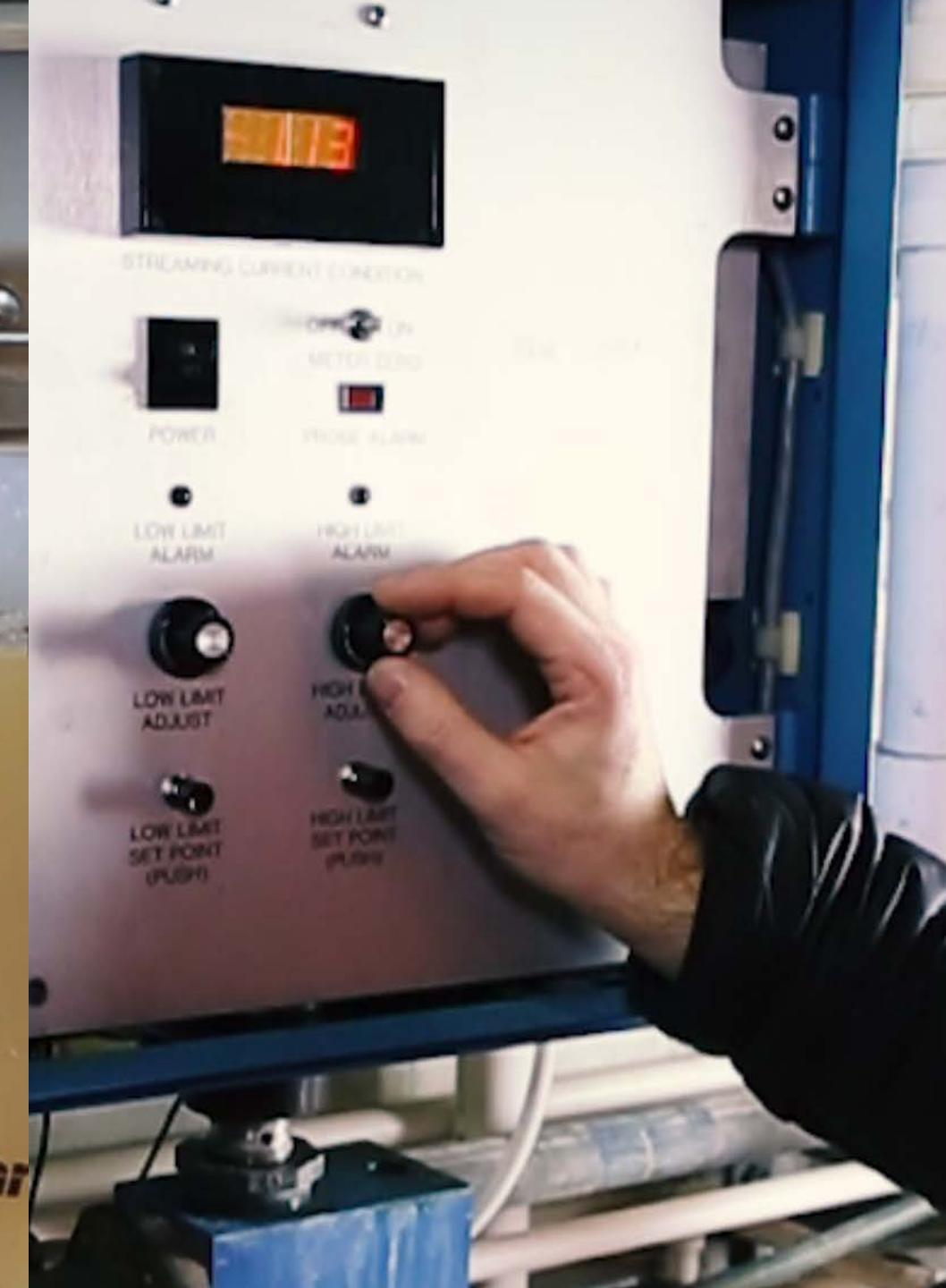
- Very hands on
- Overdosing of chemicals
- High production costs

Goals for the Project

- Improve control reliability
- Reduce production costs
- Reactive to proactive

Coagulant Dose Control

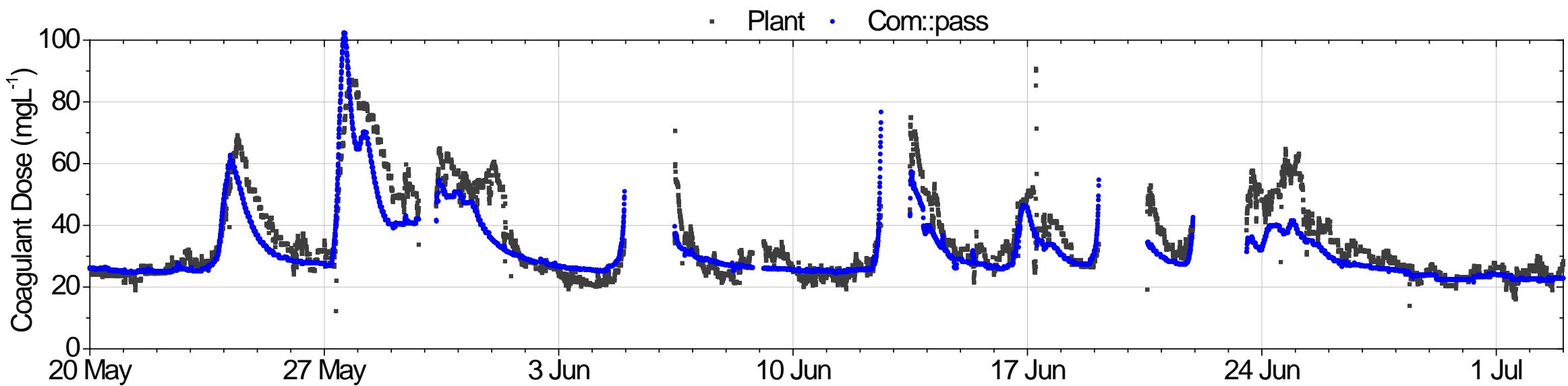






Coagulant Dose Control

- Coagulant and Lime reductions
- Filter performance improved
- More reliable



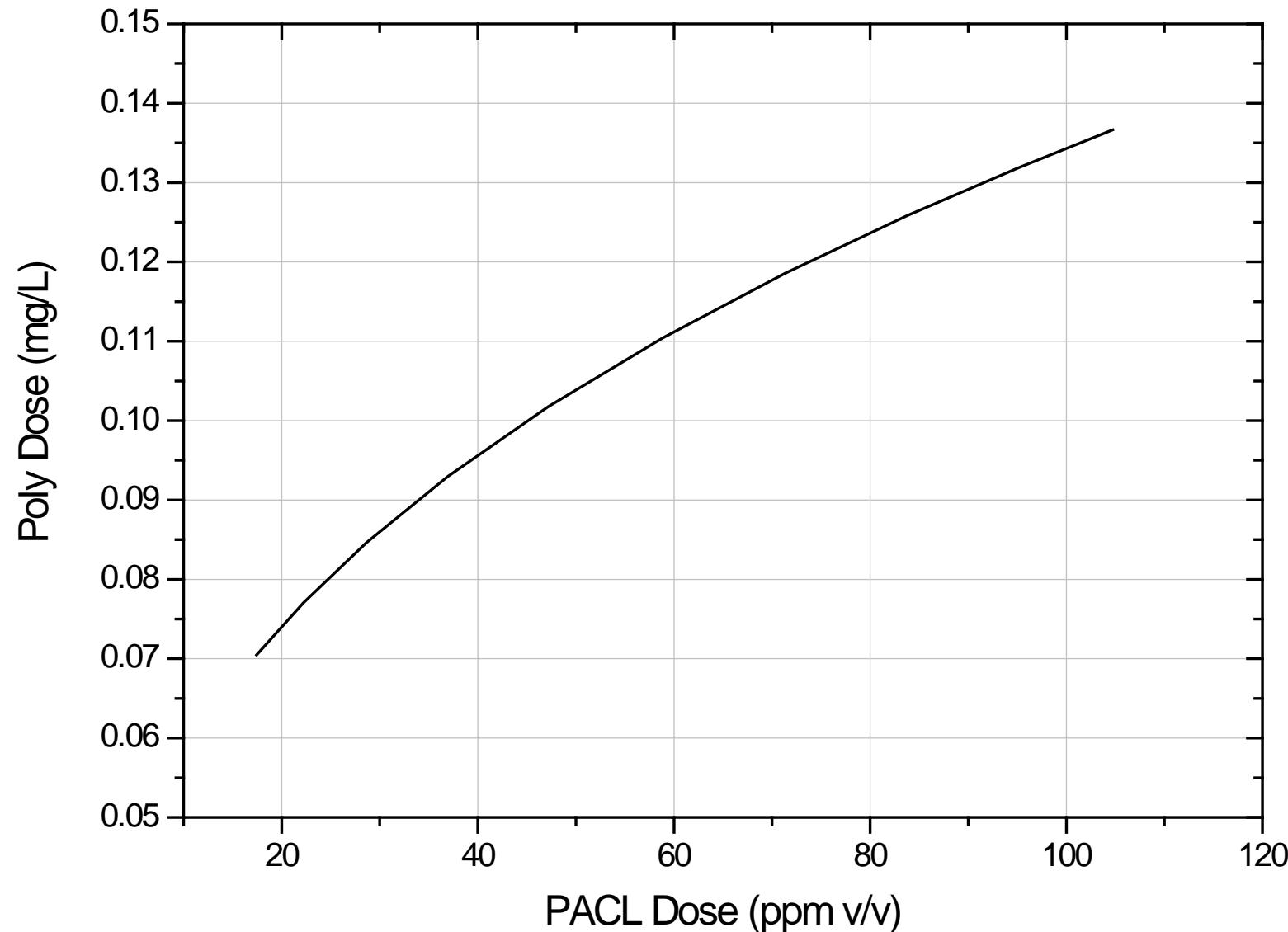
Polymer Dosing

- Setpoint control
- Too high - Carryover and filter cracking, short runtimes
- Too low – turbidity spikes
- Expensive when overdosing

To

- Automated dosing slaved off coagulant dose

Polymer Dosing



Clarifier De-sludge Control

- Time based de-sludge
- Variable solids load
- Wasting water or poor clarifier performance

To

- Load based de-sludge

Production Cost Tracking

- Bulk delivery & stock-takes
- Poor understanding
- Low transparency

To

- Online realtime production costs

Online Costs

- Chemical Costs

Equation	Description	Units
Q_{TW}	Treated water flow-rate	m^3/h <small>treated water</small>
$cost_{hypo} = \$360.40$	Product cost	$\$/m^3$ <small>product</small>
Q_{hypo}	Product flow-rate from SCADA	$L_{product}/h$
$a cost_{hypo,CWT} = \frac{24 \cdot Q_{hypo,CWT} \cdot cost_{hypo}}{100 \cdot Q_{TW}}$	Actual treatment cost	c/m^3 <small>treated water</small>

Online Costs

- Power costs

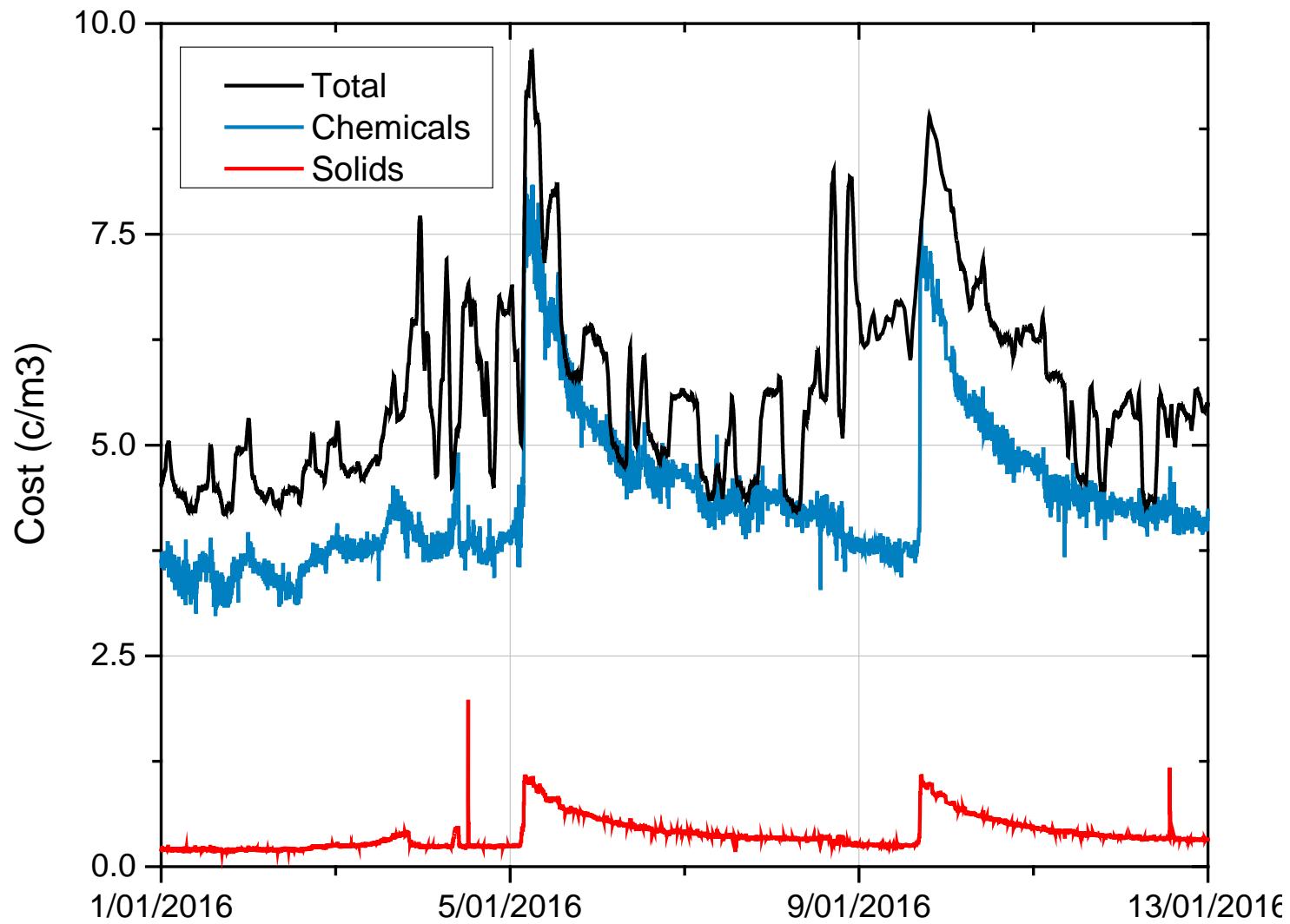


Online Costs

- Sludge disposal costs



Online Costs



Predicted Costs & Cost Sentinel

- River and inlet monitoring
- Deviation alarms
- Cost decisions

Te Marua Online Costs

	Dose Rate	Bulk Cost	Inst.Rate	Predict Rate	Last 30min	Last 24hr
CO2 Stream 1	14.830 g/m3	383.68 \$/Ton	0.581 c/m3	0.460 c/m3	0.587 c/m3	0.587 c/m3
Lime Stream 1	12.423 g/m3	322.76 \$/Ton	0.409 c/m3	1.232 c/m3	0.404 c/m3	0.316 c/m3
Poly Stream 1	0.12 g/m3	10360.00 \$/Ton	0.123 c/m3	0.207 c/m3	0.120 c/m3	0.109 c/m3
Stream 1 PAC	0.00 g/m3	2750.00 \$/Ton	0.000 c/m3	3.300 c/m3	0.000 c/m3	0.000 c/m3
Coag Stream 1	43.553 c/m3	738.22 \$/Ton	3.937 c/m3	3.480 c/m3	4.620 c/m3	3.220 c/m3
CO2 Stream 2	0.000 g/m3		0.000 c/m3		0.000 c/m3	0.000 c/m3
Lime Stream 2	0.000 g/m3		0.000 c/m3		0.000 c/m3	0.000 c/m3
Coag Stream 2	0.000 g/m3		0.000 c/m3		0.000 c/m3	0.000 c/m3
Poly Stream 2	0.000 g/m3		0.000 c/m3		0.000 c/m3	0.000 c/m3
Total Pre-Treatment			5.180 c/m3		5.731 c/m3	4.233 c/m3
Caustic	15.16 g/m3	599.13 \$/Ton	0.971 c/m3	0.719 c/m3	0.942 c/m3	0.953 c/m3
Chlorine Gas	0.84 g/m3	2964.26 \$/Ton	0.248 c/m3	0.080 c/m3	0.252 c/m3	0.251 c/m3
Hypochlorite	0.00 g/m3	334.950 \$/Ton	0.000 c/m3	0.037 c/m3	0.000 c/m3	0.000 c/m3
Fluoride	0.801 c/m3	1650.00 \$/Ton	0.134 c/m3	0.179 c/m3	0.134 c/m3	0.136 c/m3
Total Post Treatment			1.351 c/m3		1.328 c/m3	1.340 c/m3
Hutt River Predicted				0.000 c/m3	0.000 c/m3	0.000 c/m3
Plant Intake Predicted				10.751 c/m3	10.701 c/m3	9.610 c/m3
Inlet Dried Solids	15.817 g/m3					
Thickner Poly			0.033 c/m3		0.032 c/m3	0.023 c/m3
Centrifuge Poly			0.251 c/m3		0.243 c/m3	0.173 c/m3
Solids Disposal		110.00 \$/Ton	0.888 c/m3		0.861 c/m3	0.612 c/m3
Power Price		11.41 c/kWhr				
Plant Power			0.473 c/m3		0.447 c/m3	0.565 c/m3
Boost Pumps			1.056 c/m3		0.958 c/m3	0.854 c/m3
Treatment Pumps			0.000 c/m3		0.000 c/m3	0.000 c/m3
PAT Saving			0.000 c/m3		0.000 c/m3	0.000 c/m3
Totals						
Total Chemical			6.532 c/m3		7.059 c/m3	5.573 c/m3
Total Power			1.509 c/m3		1.406 c/m3	1.419 c/m3
Total Solids			1.144 c/m3		1.138 c/m3	0.808 c/m3
All Cost Total			8.941 c/m3		9.601 c/m3	7.800 c/m3



CO2	PAC	CL2	FL
12.000 %/vol	12.000 g/m3	0.800 g/m3	0.750 g/m3

Calibration Factors	
Lime Feeder A	1.0700
Lime Feeder B	1.0700
Lime Feeder C	
Poly Strength	0.30 %w/vol
Hypo Strength	0.77 %w/vol
Plant Recovery	98.0 %
Thickner Dose	2.0 kg/TonDS
Cent. Dose	15.0 kg/TonDS
Sludge Cake DS	20.00 % w/v

- Trends**
- Plant Volumes
 - Stream 1
 - Stream 2
 - Post Treatment
 - Solids
 - Power
 - Totals

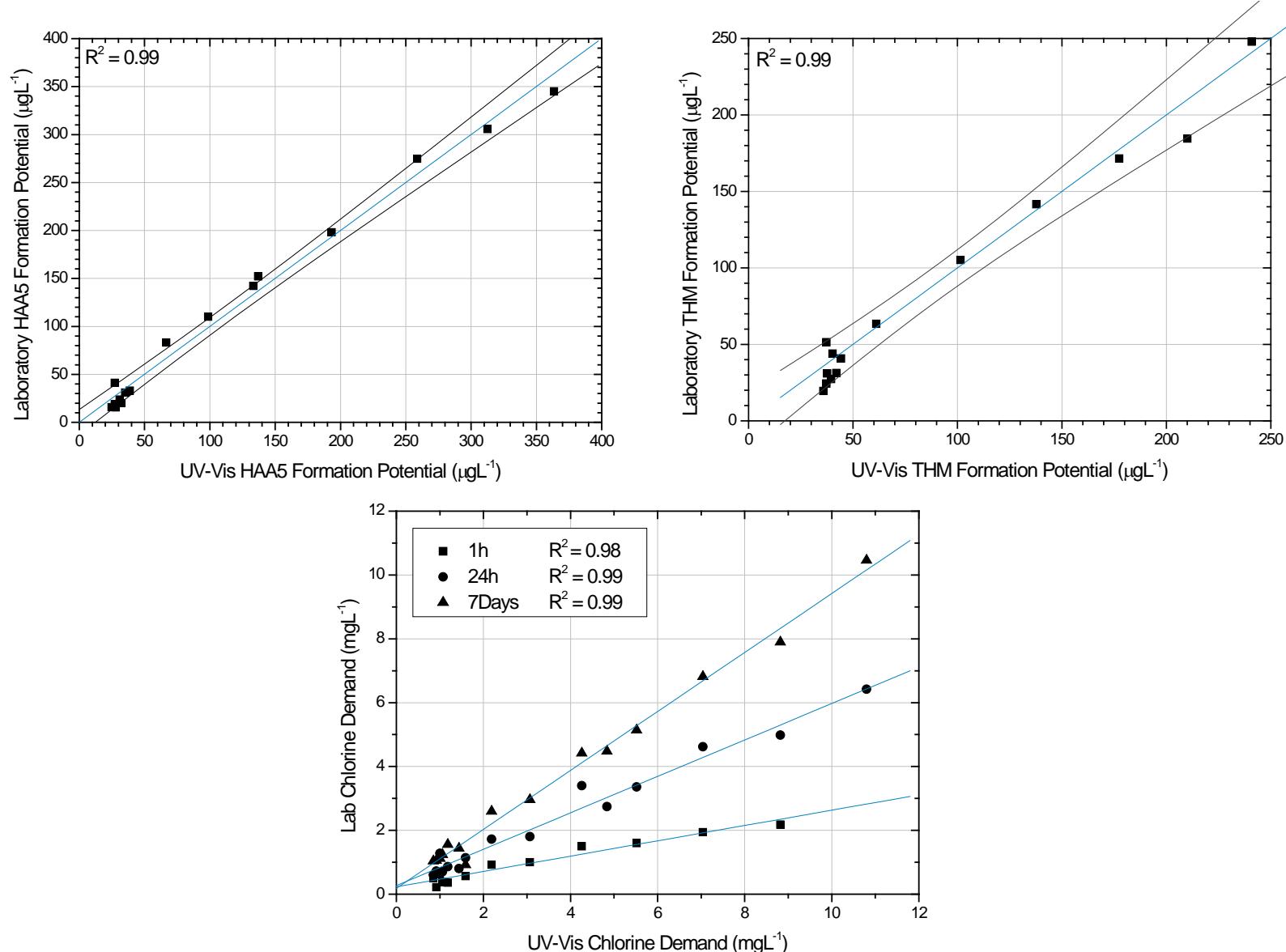
Alkalinity Control

- Manual CO₂ dose control
- Variable treated water alkalinity

To

- Feed forward alkalinity control
- Tightly controlled treated water alkalinity

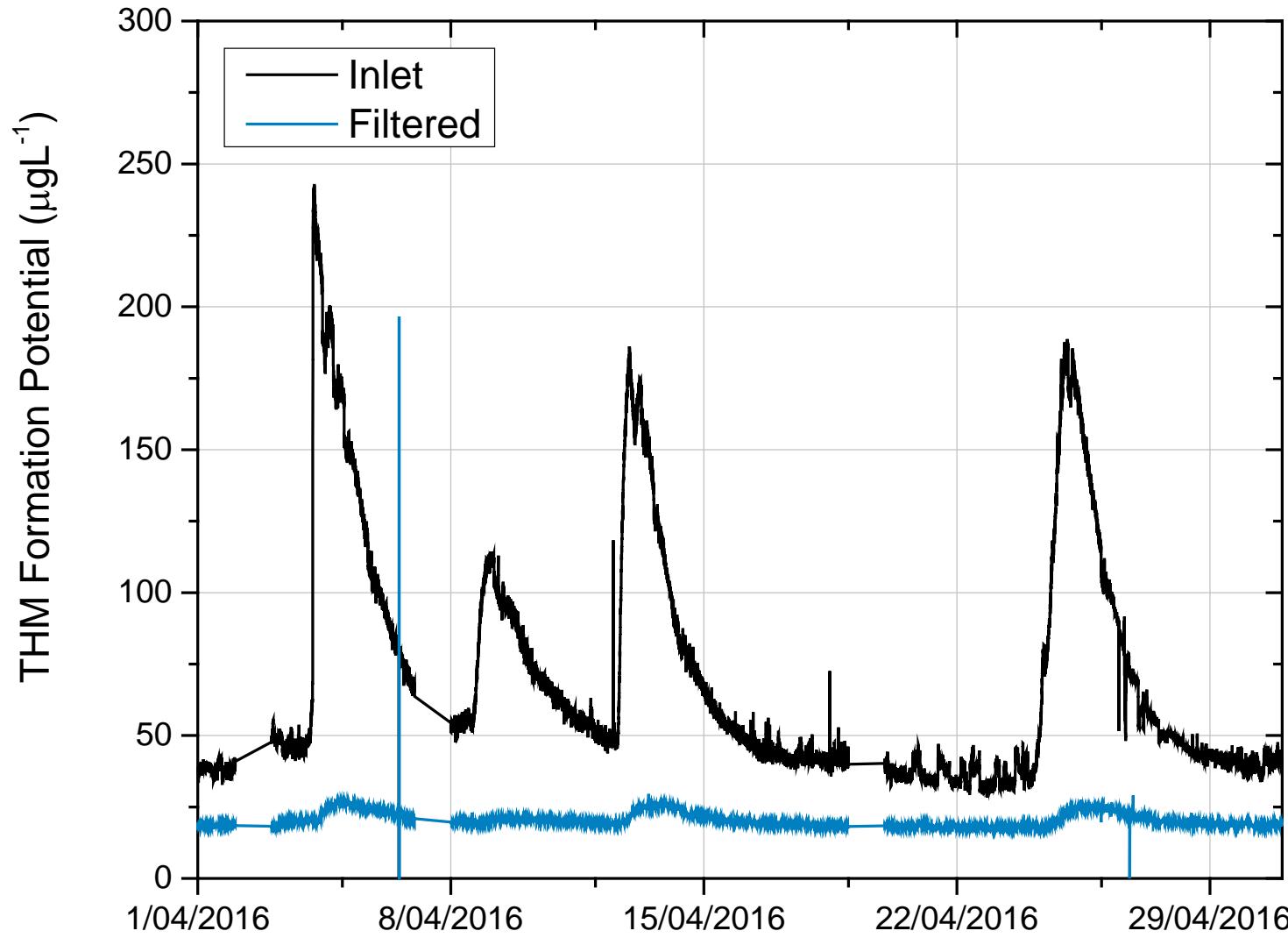
Chlorine Demand and THM/HAA FP



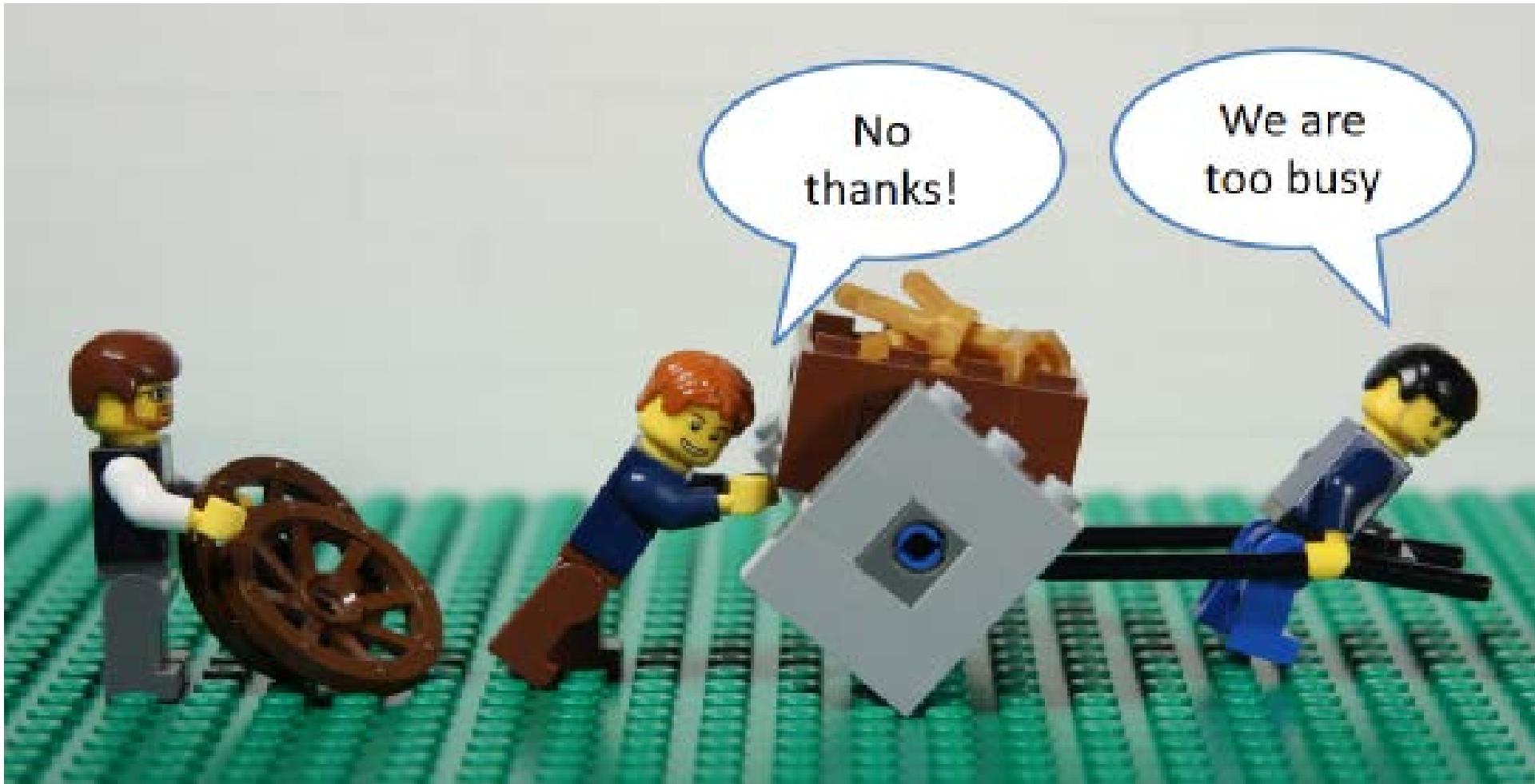
Chlorine Demand and THM/HAA FP

- Online Measurement
- P2 risk reduction
- Optimisation potential

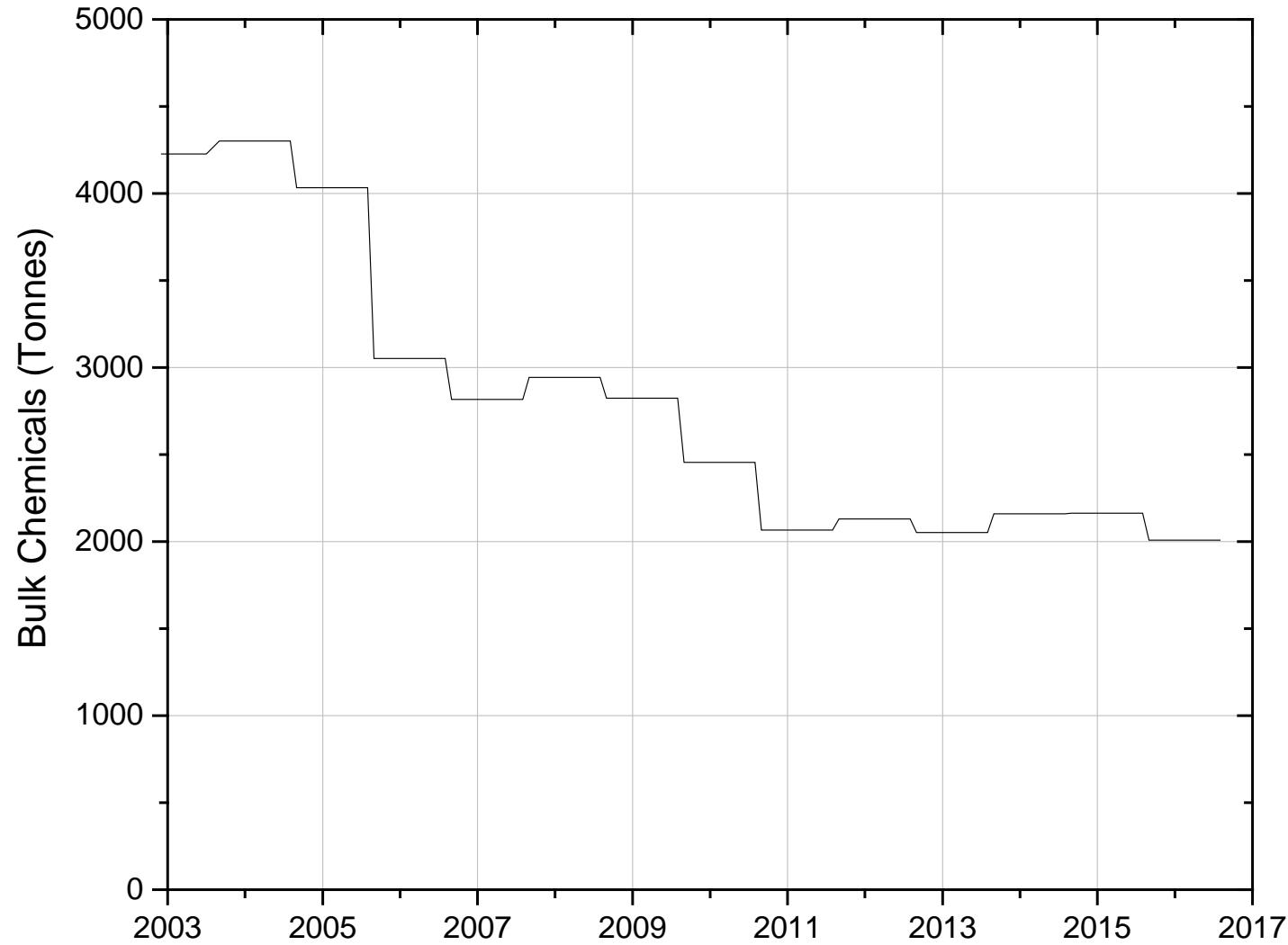
Enhanced Organics Removal



Conclusion



Conclusion



Questions?

