## Pressure Management and Fire Supplies from a Network Perspective



© Thomas Consultants Limited 2023. This presentation and document is the property of Thomas Consultants Limited and may not be copied; recorded or stored by electronic, magnetic, electromagnetic or other process or otherwise in a machine readable form; translated from the original form; recompiled; made into a compilation; partially copied; modified; updated or otherwise altered without the express written permission of Thomas Consultants Limited.

#### Drinking Water Protection Conference 1 & 2 August 2023

Presentation by Richard Taylor, Thomas Consultants Ltd, Auckland



#### Water Supply – Levels of Service

#### Key Service Areas and Levels of Service:

- Water quality Meet the requirements of the Drinking Water Standards for NZ
- Supply flow and pressure 25 litres/min and <u>250 kPa (at the meter)</u>, meet NZ Fire Service Code of Practice hydrant flows
- Continuity of supply Reliability of the network (condition, number of network faults), Response to Faults/Complaints
- Adequacy of Supply Efficient use of water, water loss, drought standards









#### Water Supply – Levels of Service

#### QUESTION

Do you know what your Council's level of service is for supply pressure?





#### **Typical Water Supply System**



This town (Balclutha population 4,000) has watermains 50mm – 300mm diameter (NB).



#### **Example of a Medium Water Supply System**

#### **BULK MAIN AND CITY RESERVOIRS**



# Hamilton, population 185,000

#### Has a 620mm NB Ring Main



#### **General Layout – Showing Typical Street (ex GIS)**





#### General Layout – Example Showing the Typical Interconnectivity Between Watermains (ex GIS)



thomas

consultants

#### **PIPELINE SYSTEMS – Pressure or Gravity?**



Gravity systems rely on <u>water flowing downhill</u>, and pipelines are designed to run <u>part full</u> or <u>'just full</u>' (or they surcharge). <u>Pipelines are laid</u> to a grade between manholes.

Water supply networks are <u>pressure systems</u>. The pipes are <u>always full</u> and <u>under pressure</u>. Water can flow uphill and downhill driven by 'pressure'. But there are friction losses (or <u>headlosses</u>) as water travels through the pipes.



#### **Concept of Hydraulic Grade Line**



Water held at an elevation is stored energy. Hydro schemes convert some of this energy into electricity.

Pump stations work in reverse – electricity is used to 'elevate' water.

The 'stored' or 'potential energy' of water can be expressed as an elevation (i.e. in metres) as the Hydraulic Grade Line (HGL). <u>Due to the friction losses (headlosses) occurring with flow in a pipeline, the HGL of the water reduces as it travels along the pipeline</u>.

#### **Example of Hydraulic Grade Line**



- The Static Pressure (with no flow or headlosses) is at a HGL is 92m
- With Demand (i.e. water use) the HGL reduces due to headlosses i.e Dynamic Pressure line



#### **Example of Hydraulic Grade Line & Pressure M/ment**



- The Static Pressure (with no flow or headlosses) is at a HGL is 92m
- With Demand (i.e. water use) the HGL reduces due to headlosses
- With Pressure Management PRV's 'step down' the HGL (pressure)



#### Water Networks – Calculating Pressure

The water pressure at a property is calculated as follows:

The HGL (at the location) – Ground Elevation = Pressure at the property

i.e. 92m (HGL) – 40m (Ground Elevation) = 52m Pressure (or 520 kPa)



# Why do Water Suppliers reduce supply pressures?





### **Benefits of Pressure Management**

- The level of leakage is reduced immediately!
- The 'Rate of Rise' of leakage in the network is reduced
- Watermain burst rates will be reduced (with cost and customer service benefits)
- The 'loss of water' from every burst and leak will be reduced
- The 'life expectancy' of watermains and service pipe assets will be extended - watermain renewal programmes can be extended and depreciation costs reduced
- Customer pressure-related water demand is reduced
- Less stress on private plumbing (less private leaks)





### **Fire Sprinkler Systems**

What I've Learnt

- Fire Engineering is a specialist field of engineering
- Communication between civil/water supply' engineers and fire engineers is generally unsatisfactory and problematic
- Water supply issues with fire sprinkler systems are MAJOR issues (building won't get compliance, new buildings can't be occupied or insured)





### Fire Sprinkler Systems – Key Features

#### <u>Sprinkler Valve Room</u> (SVR), <u>Water Connection</u> (with Detector Check Valve and metered bypass) and the '<u>Block Sheet</u>' (showing the design points)







#### Fire Sprinkler Systems – Block Sheet





#### **Fire Sprinkler Systems – Block Sheet (Water Supply Graph)**

Sprinkler system

Water supply results

Water supply results

Sprinkler system demands plotted

Sometimes a site plan



<u>Fire Protection Inspection Services Limited</u> 10281 CATHERINE COURT REST HOME 19 DENVER AVE, HENDERSON, AUCKLAND

12/11/08

Fire Protection Inspection Services Limited 4-6420-B WOOL EQUITIES, 11-17 EDWARD STREET, MILTON

2/07/2015

#### WATER SUPPLY GRAPH

| Client/Prem<br>Address:<br>Flow Taken<br>Flow Meter<br>Reference C | Client/Premises:<br>Address:<br>Flow Taken At:<br>Flow Meter No.:<br>Reference Gauge No.: |                                  | Catherine Court Rest Home<br>19 Denver Ave, Henderson, Auckland<br>Test Point<br>Res2<br>H996 |                         |       | Date:<br>Filecode(s):<br>Hazard Classifications:<br>Hydraulic Demands: |         |           | 12/11/08<br>10281<br>*RES<br>45 l/min @ 84 kPa<br>115 l/min @ 91 kPa<br>0 l/min @ 0 kPa<br>0 l/min @ 0 kPa |  |
|--|---|----------------------------------|---|-------------------------|-------|--|---------|-----------|--|--|
|  |   | PRIMA                            | RY  |                         |       |  |         |           |  |  |
| This is town   | s a single<br>main, with  | water supp<br>a 50mm co<br>valve | ly from the De<br>onnection to th<br>s.   | enver Ave<br>ae control |       |  |         |           |  |  |
|  |   | Time Take                        | n: 0945   |                         |       |  | Time Ta | ken:      |  |  |
| Flow   | and some  | Pres                             | sure kPa  |                         | Flow  |  | Pres    | sure kPa  |  |  |
| Ilmin  | Inst.   | Suction                          | Discharge   | RPM                     | l/min | Inst.  | Suction | Discharge | RPN  |  |
| Drain  | 360   | 0                                | 0   | 0                       | Drain | 0  | 0       | 0         | 0  |  |
| 0  | 470   | 0                                | 0   | 0                       | 0     | 0  | 0       | 0         | 0  |  |
| 50   | 440   | 0                                | 0   | 0                       | 0     | 0  | 0       | 0         | 0  |  |
| 100  | 430   | 0                                | 0   | 0                       | 0     | 0  | 0       | 0         | 0  |  |
| 150  | 400   | 0                                | 0   | 0                       | 0     | 0  | 0       | 0         | 0  |  |
| 200  | 370   | 0                                | 0   | 0                       | 0     | 0  | 0       | 0         | 0  |  |
| 0  | 0   | 0                                | 0   | 0                       | 0     | 0  | 0       | 0         | 0  |  |
| Test   | 0   | 0                                | 0   | 0                       | Test  | 0  | 0       | 0         | 0  |  |
|  | 570<br>513<br>456   | 70 440-                          |   | 39                      |       |  |         | FRIMAR    | -  |  |



| Client/Premises:<br>Valve House Name:<br>Address:<br>Flow Taken At:   |  | Woo  | Wool Equities  |  | Date:  | 2/07   | 2/07/2015  |   |   |  |
|---|--|--|--|--|--|--|--|---|---|--|
|   |  | Woo  | I Equities   |  | Physical Fi                                    | Physical File:   |  | 4-6420-B  |   |  |
|   |  | 11-1   | 7 Edward St  | reet, Milton   | Hazard Classifications:                        |  |  | OH3   |   |  |
|   |  | FSI  |  |  | Hydraulic C                                    | 135<br>135<br>135  | 1350 l/min @ 423 kPa<br>1350 l/min @ 255 kPa<br>1350 l/min @ 282 kPa   |   |   |  |
| low Meter   | No.:   | GHF  | P44  |  |  |  |  |   |   |  |
| eference Gauge No.:   |  | WG   | TN HP2   |  |  |  |  |   |   |  |
|   |  | PRIMARY  |  |  |  |  | ECONDAR  | IY  |   |  |
| This is a 'C  | lass A' wat  | er supply (F   | OC rules). T   | he primary   | a seco   | riuary oupp  | iy is from a   | Electric Mo   | tor driven  |  |
| This is a 'C<br>supply is fi<br>capacity (  | lass A' wat<br>rom the per<br>of 45,000 II<br>Time   | er supply (F<br>trol motor fin<br>tres and aut<br>Taken: 10.   | OC rules). The pump with<br>omatic top-u   | a storage<br>p facility.   | pumpse   | t with a stor<br>autom   | age capacity<br>attic top up 1<br>Time Taken   | y of 90,000 li<br>facility.   | tres and  |  |
| This is a 'C<br>supply is fi<br>capacity (<br>Flow  | lass A' wat<br>rom the pet<br>of 45,000 li<br>Time   | er supply (F<br>trol motor fin<br>tres and aut<br>Taken: 10.<br>Pressu   | OC rules). Tr<br>e pump with<br>omatic top-u<br>00am<br>ure kPa  | he primary<br>a storage<br>p facility.   | Flow   | t with a stor<br>autom   | age capacity<br>atic top up t<br>Time Taken<br>Pressu  | y of 90,000 li<br>facility.<br>I:<br>ure kPa  | tres and  |  |
| This is a 'C<br>supply is fi<br>capacity of<br>Flow<br>Vmin   | lass A' wat<br>rom the per<br>of 45,000 li<br>Time<br>Inst.  | er supply (Fi<br>trol motor fin<br>tres and auti<br>Taken: 10.<br>Pressu<br>Suction  | OC rules). Tr<br>e pump with<br>omatic top-u<br>00am<br>ure kPa<br>Discharge   | RPM  | Flow<br>Umin                                   | inst.  | age capacit<br>natic top up<br>Time Taker<br>Press   | of 90,000 li<br>facility.<br>In:<br>ure kPa<br>Discharge  | RPM   |  |
| This is a 'C<br>supply is fi<br>capacity of<br>Flow<br>Winin<br>Drain   | lass A' wat<br>rom the per<br>of 45,000 II<br>Time<br>Inst.<br>0   | er supply (F<br>trol motor fin<br>tres and aut<br>e Taken: 10.<br>Pressu<br>Suction<br>0   | OC rules). Tr<br>e pump with<br>omatic top-u<br>00am<br>ure kPa<br>Discharge<br>0  | RPM<br>0   | Flow<br>Umin<br>Drain                          | Inst.  | Time Taken<br>Suction  | y of 90,000 li<br>facility.<br>I:<br>ure kPa<br>Discharge<br>0  | RPM<br>0  |  |
| This is a 'C<br>supply is fi<br>capacity of<br>Flow<br>Umin<br>Drain<br>0                                       | lass A' wat<br>rom the per<br>of 45,000 II<br>Time<br>Inst.<br>0<br>530                                  | er supply (F<br>trol motor fin<br>tres and aut<br>taken: 10.<br>Pressu<br>Suction<br>0<br>0  | OC rules). Ti<br>e pump with<br>omatic top-u<br>00am<br>ure kPa<br>Discharge<br>0<br>0   | RPM<br>0   | Flow<br>Umin<br>Drain<br>0                     | Inst.  | Time Taker Presst Suction 0 0  | v of 90,000 li<br>facility.<br>It:<br>Discharge<br>0<br>0   | RPM<br>0  |  |
| This is a 'C<br>supply is fi<br>capacity of<br>Flow<br>Umin<br>Drain<br>0<br>600                                | lass A' wat<br>rom the pel<br>of 45,000 II<br>Time<br>Inst.<br>0<br>530<br>500                           | er supply (F<br>trol motor fin<br>tres and aut<br>Taken: 10.<br>Pressu<br>Suction<br>0<br>0<br>0   | OC rules). Ti<br>e pump with<br>ormatic top-u<br>00am<br>ure kPa<br>Discharge<br>0<br>0<br>0                                     | RPM<br>0<br>0  | Flow<br>Umin<br>Drain<br>0                     | Inst.  | Time Taker Press Suction 0 0 0   | v of 90,000 li<br>facility.<br>It:<br>Discharge<br>0<br>0<br>0  | RPM<br>0<br>0   |  |
| This is a 'C<br>supply is fi<br>capacity of<br>Flow<br>Umin<br>Drain<br>0<br>600<br>1000                        | lass A' wat<br>rom the per<br>of 45,000 II<br>Time<br>Inst.<br>0<br>530<br>500<br>440                    | er supply (F<br>troi motor fin<br>tres and aut<br>e Taken: 10.<br>Pressu<br>Suction<br>0<br>0<br>0<br>0<br>0   | OC rules). Ti<br>e pump with<br>omatic top-u<br>00am<br>ure kPa<br>Discharge<br>0<br>0<br>0<br>0                                 | RPM<br>0<br>0<br>0<br>0  | Flow<br>Limin<br>Drain<br>0<br>0               | Inst.<br>0<br>0<br>0   | age capacity<br>astic top up i<br>Time Taken<br>Pressu<br>Suction<br>0<br>0<br>0   | v of 90,000 II<br>facility.<br>I:<br>Discharge<br>0<br>0<br>0<br>0<br>0   | RPM<br>0<br>0<br>0  |  |
| This is a 'C<br>supply is fi<br>capacity of<br>Flow<br>Umin<br>Drain<br>0<br>600<br>1000<br>1400                | lass A' wat<br>rom the pel<br>of 45,000 II<br>Time<br>Inst.<br>0<br>530<br>500<br>440<br>460             | er supply (F<br>troi motor fin<br>tres and aut<br>tres and<br>tres | OC rules). Ti<br>e pump with<br>omatic top-u<br>00am<br>Discharge<br>0<br>0<br>0<br>0<br>0<br>0                                  | RPM<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0                               | Flow<br>Umin<br>Drain<br>0<br>0<br>0<br>0      | Inst.<br>0<br>0<br>0<br>0  | age capacity<br>add capacity<br>attic top up i<br>Time Taken<br>Pressu<br>Suction<br>0<br>0<br>0<br>0  | y of 90,000 li<br>facility.<br>It:<br>Discharge<br>0<br>0<br>0<br>0<br>0<br>0<br>0                                    | RPM<br>0<br>0<br>0<br>0<br>0  |  |
| This is a 'C<br>supply is fi<br>capacity of<br>Flow<br>Umin<br>Drain<br>0<br>600<br>1000<br>1400<br>0           | lass A' wat<br>rom the pel<br>of 45,000 li<br><b>Time</b><br>1nst.<br>0<br>530<br>500<br>440<br>460<br>0 | resupply (Fi<br>troi motor fin<br>ters and aut<br>Taken: 10.<br>Pressu<br>Suction<br>0<br>0<br>0<br>0<br>0<br>0<br>0   | OC rules). Ti<br>e pump with<br>omatic top-u<br>00am<br>Discharge<br>0<br>0<br>0<br>0<br>0<br>0<br>0                             | RPM<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | Flow<br>Umin<br>Drain<br>0<br>0<br>0<br>0      | Inst.<br>0<br>0<br>0<br>0<br>0<br>0  | Time Taken Pressi Suction 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  | v of 90,000 li<br>facility.<br>v re kPa<br>Discharge<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | RPM<br>0<br>0<br>0<br>0<br>0<br>0<br>0                                    |  |
| This is a 'C<br>supply is fi<br>capacity of<br>flow<br>Umin<br>Drain<br>0<br>0<br>000<br>1000<br>1400<br>0<br>0 | lass A' wation the peich<br>of 45,000 II<br>Time<br>Inst.<br>0<br>530<br>530<br>440<br>460<br>0<br>0     | er supply (F.<br>trol motor fin<br>tres and autor<br>traken: 10.<br>Pressu<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0  | OC rules). Ti<br>e pump with<br>omatic top-u<br>00am<br>are kPa<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | RPM<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | Flow<br>Umin<br>Drain<br>0<br>0<br>0<br>0<br>0 | Instruction of the store of the | y is from a lage capacity<br>adic top up i<br>Time Taken<br>Pressi<br>Suction<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | y of 90,000 li<br>facility.<br>It<br>Discharge<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0  | RPM<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 |  |

WATER SUPPLY GRAPH

#### <u>NOTE</u> – A PUMP generally means network pressure is not critical





WATER SUPPLY WAS INADEQUATE FOR THE DEMANDS AT THIS SPECIFIC TIME AND DATE ONLY. FLUCTUATIONS DO OCCUR THAT CONTRACTORS SHOULD BE AWARE OF.

### **Fire Sprinkler Systems – Head Losses**

Headlosses occur in all of the following areas. It is important to understand this with design and/or dealing with issues:

- Losses in the public network up to the connection point (at the boundary)
- Head losses through the detector check valve
- Losses on the internal watermain to the SVR
- Losses through the valves (including non-return valve) in the SVR
- Losses in the sprinkler system pipework from the SVR to the sprinkler head
- Losses through the sprinkler head itself





#### **Metering of a Fire Sprinkler System**



#### Flow direction is Right to Left



#### **Graphs of Headloss through a Detector Check Valve**

fps

mps

fns

mps

#### Capacity

Rated working pressure 175psi (12.06 bar) \* Rated flow \*\*UL Tested



#### Typically around 4 psi = 28 kPa (but varies 2 - 6psi = 14 - 40 kPa)

#### And for a Reduced Pressure Zone Device ....



#### Graphs of Headloss for an <u>Reduced Pressure Zone</u> (RPZ) Device

Capacity \*Typical maximum flow rate (7.5 feet/sec.)







### **Typically around** 10-12 psi = 70 - 80 kPa



#### Water Services Act 2021

#### 27 Duty to protect against risk of backflow

- If a drinking water supply includes reticulation, the drinking water supplier must ensure that the supply arrangements
  protect against the risk of backflow.
- (2) If there is a risk of backflow in a reticulated drinking water supply, the drinking water supplier may-
  - (a) install a backflow prevention device and require the owner of the premises to reimburse the supplier for the cost of installation, maintenance, and ongoing testing of the device; or
  - (b) require the owner of the premises to install, maintain, and test a backflow prevention device that incorporates a verifiable monitoring system in accordance with any requirements imposed by the supplier.
- (3) A person who installs a backflow protection device must take all reasonable steps to ensure it operates in a way that does not compromise the operation of any fire extinguisher system connected to the drinking water supply. Compare: 1956 No 65 a 69ZZZ

My view is that water suppliers can control/reduce supply pressures but must give reasonable notice so building owners have time to make necessary changes/adjustments



# Example of a Fire Sprinkler System Issue in Rotorua (supermarket)



Sprinkler system has a hydraulic demand of 40.2 litres/sec (at 415 kPa).

This flowrate through a 100mm road crossing (and 100mm B/F assembly I think) is unsatisfactory (Velocity > 5 m/s).

Upsizing of the road crossing (and the B/F assembly, and possibly the internal main) is required. thomas

### **Fire Sprinkler Systems – Final Comments**

Some final thoughts:

- The flow available at the Sprinkler Valve Room is physically checked annually. <u>Non-compliance can be</u> <u>caused by network valves being left in the 'OFF</u>' <u>position</u> after maintenance work.
- My information from the 1990's was that the '80% allowable' figure was based on 10% daily fluctuation in (street) pressure and 10% future long term deterioration in pressure with 'growth' in demand. I was advised that within a pressure managed area/zone, the latter 10% could be disregarded, and hence 90% allowable pressure was acceptable (to the Insurance Council)







# **Any Questions?**

richard.taylor@tcec.co.nz

